

# Journal of Biomedical Optics

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## **Graphics processing unit accelerated intensity-based optical coherence tomography angiography using differential frames with real-time motion correction**

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# Graphics processing unit accelerated intensity-based optical coherence tomography angiography using differential frames with real-time motion correction

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**Abstract.** We demonstrate intensity-based optical coherence tomography (OCT) angiography using the squared difference of two sequential frames with bulk-tissue-motion (BTM) correction. This motion correction was performed by minimization of the sum of the pixel values using axial- and lateral-pixel-shifted structural OCT images. We extract the BTM-corrected image from a total of 25 calculated OCT angiographic images. Image processing was accelerated by a graphics processing unit (GPU) with many stream processors to optimize the parallel processing procedure. The GPU processing rate was faster than that of a line scan camera (46.9 kHz). Our OCT system provides the means of displaying structural OCT images and BTM-corrected OCT angiographic images in real time. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: [10.1117/1.JBO.19.2.021105](https://doi.org/10.1117/1.JBO.19.2.021105)]

Keywords: optical coherence tomography; angiography; graphics processing unit.

Paper 130172SSR received Mar. 26, 2013; revised manuscript received May 27, 2013; accepted for publication Jun. 21, 2013; published online Jul. 11, 2013.

## 1 Introduction

Optical coherence tomography (OCT) is a noncontact, noninvasive imaging modality that can provide high-resolution, depth-resolved imaging of internal microstructures within the tissue.<sup>1</sup> The development of Fourier domain optical coherence tomography, which provides markedly increased imaging speeds and high sensitivity,<sup>2,3</sup> has enabled *in vivo* imaging of blood flow. Recent technological advances in OCT-based flow imaging techniques can be grouped into two categories: Doppler OCT and OCT angiography. Phase-resolved Doppler OCT uses the phase difference between adjacent A-lines to extract the Doppler frequency shift and quantitative information, such as blood flow speed and direction.<sup>4–8</sup> The power of Doppler shift images and phase variance images can be used to construct OCT angiograms for vasculature visualization.<sup>9,10</sup> For bulk-tissue-motion (BTM) on the order of a wavelength, which is much smaller than the axial resolution, the effect of motion appears as a phase shift. A number of methods for bulk-phase correction have been proposed.<sup>7,10</sup>

Intensity-based (IB) methods of imaging blood vessels have been proposed.<sup>11–17</sup> These methods are insensitive to bulk-phase changes, and therefore, do not require bulk-motion phase correction.<sup>14</sup> Interframe (IF) flow-imaging techniques have been used to detect microvasculature.<sup>12,13,15–17</sup> IF speckle variance images were calculated across three structural OCT images of nude mice.<sup>12</sup> The vasculature network in human skin was imaged using a four-frame IF-IB Doppler variance (DV) method.<sup>16</sup> As the number of frames increases, the signal-to-noise ratio (SNR) improves; however, this approach also increases the sensitivity of these methods to bulk motion (on

the order of a pixel). Therefore, IF methods are suitable for imaging fixed samples, or for use with higher frame rates; otherwise, the method requires BTM correction on the order of a pixel.

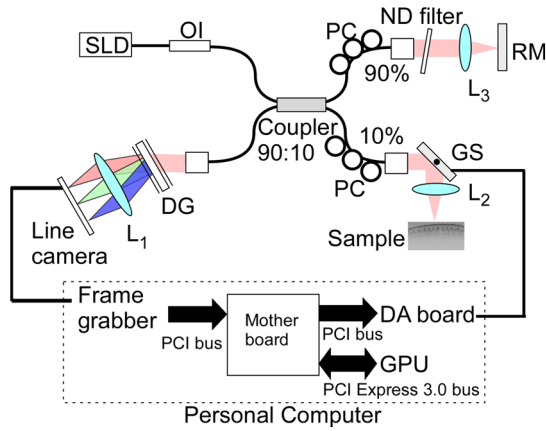
Real-time display of tissue structure and flow information is always desirable for clinical applications that require immediate diagnosis for screening or biopsy/surgery. Our group and others have demonstrated real-time processes and the display of structural OCT images using a graphics processing unit (GPU).<sup>18–23</sup> The GPU has many processors that provide highly parallel computing at a low cost, with the advantage of simple programming on a host computer. GPU processing is capable of displaying both structural OCT and Doppler OCT images in real time (e.g., Doppler OCT using the Kasai autocorrelation algorithm,<sup>24</sup> speckle variance with BTM correction,<sup>25</sup> and phase-resolved four-dimensional Doppler OCT<sup>26</sup>).

In this paper, we demonstrated GPU-accelerated IB-OCT angiography, using two sequential frames with a simple BTM correction. The squared difference between two sequential amplitudes of the OCT images was used to minimize motion artifacts. We chose the BTM-corrected image that minimized the sum of the pixel values, from a total of 25 calculated OCT angiographic images, using axial- and lateral-pixel-shifted structural OCT images. A GPU processing rate of more than 100,000 lines/s exceeded the line rate of the camera (46.9 kHz). Thus, our OCT system could display structural OCT images and BTM-corrected OCT angiography in real time.

## 2 Experimental Setup

Figure 1 shows a schematic diagram of our FD-OCT system. A superluminescent diode (central wavelength: 1330 nm; spectral bandwidth: 58 nm) was used to illuminate the system. A polarization-independent fiber isolator was placed immediately after the light source to avoid light reflection into the source. The light was split into sample and reference beams, with the latter being terminated by a mirror using a 90/10 fiber coupler.

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**Fig. 1** Schematic of spectral domain optical coherence tomography. SLD, superluminescent diode; OI, optical isolator; L, achromatic lens; ND filter, neutral density filter; PC, polarization controller; DG, diffraction grating.

Achromatic lenses ( $f = 45$  mm) were inserted into both beam trajectories to compensate for the dispersion mismatch. Light returning from the reference mirror and sample were recombined in the fiber coupler. The output interference spectra were detected by a custom-built spectrometer, comprising a 35-mm focal-length achromatic collimating lens, a 1145-lines/mm transmission grating (Wasatch Photonics, Logan, Utah), and a 100-mm focal-length achromatic lens. The spectra were focused onto a line-scan InGaAs camera (Goodrich-Sensors Unlimited, 1024 pixels, 14-bit resolution) operated at 46.9 kHz. The camera output was fed to a personal computer (PC) via a low-cost camera-link board (National Instruments, Austin, Texas, PCI-1426, 16-bit resolution).

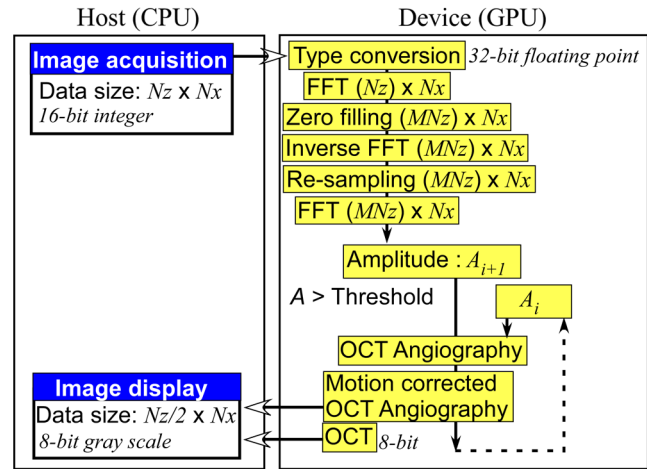
Signal processing was performed using a graphics card (Nvidia, Santa Clara, California, GeForce GTX680, 1006-MHz processor clock, 1536 stream processors, and 2048 Mbytes GDDR5 memory). This graphics card was connected to the host computer via a PCI-Express 3.0  $\times$  16 interface, which had twice the data transfer rate compared with the previous work.<sup>20</sup> We used Nvidia's compute unified device architecture (CUDA) Version 4.2,<sup>27</sup> which could be programmed in C language to exploit the processing power of the GPUs. We developed software that included image acquisition, GPU programming, and a graphical user interface environment in the Microsoft Visual C++2008 Express Edition.

### 3 OCT Angiography Using a GPU

Multiple frames-based OCT angiography is susceptible to BTM and requires an increase in the number of acquired frames to improve the SNR. To minimize motion artifacts, we used two sequential frames and averaged the amplitudes in both the lateral and depth directions. The algorithm that we developed for this purpose is given below by Eq. (1):

$$\text{OCTA}_{i,j,k} = \frac{\sum_{j=1}^J \sum_{k=1}^K (A_{i,j,k} - A_{i+1,j,k})^2}{\sum_{j=1}^J \sum_{k=1}^K (A_{i,j,k}^2 + A_{i+1,j,k}^2)}, \quad (1)$$

where  $A_{i,j,k}$  is the amplitude of the OCT image and  $i$ ,  $j$ , and  $k$  are indices for the frame, transverse, and depth pixels, respectively.  $K$  is the number of averaged depth pixels and  $J$  is the number of averaged A-lines. Pixel-shifted images were used to correct for



**Fig. 2** Flow chart of GPU programming of FD-OCT and intensity-based OCT angiography using two frames.

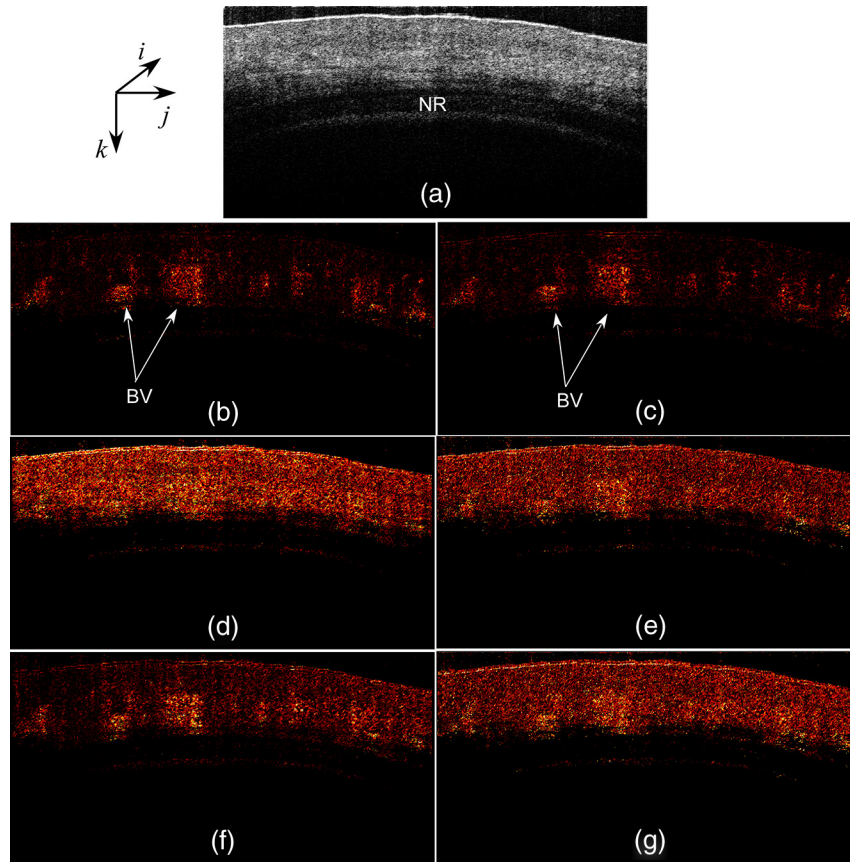
BTM. This correction is accounted for in the modified version of Eq. (1), given below in Eq. (2):

$$\text{OCTA}_{i,j,k} = \frac{\sum_{j=1}^J \sum_{k=1}^K (A_{i,j,k} - A_{i+1,j+p,k+q})^2}{\sum_{j=1}^J \sum_{k=1}^K (A_{i,j,k}^2 + A_{i+1,j+p,k+q}^2)}, \quad (2)$$

where  $p$  and  $q$  are the pixel translations of the lateral and depth directions, respectively. Because we could not predict the direction of tissue motion, we calculated the squared difference of two OCT images by changing  $p$  and  $q$ , to find the shift values that minimized the sum of the pixel values. Generally, larger  $J$  and  $K$  values for the averaging will increase image SNR; however, it also increases the computation time and results in a “blurring” and loss of smaller vessels. The larger  $p$  and  $q$  values for the image registration will increase the computation time. To display BTM-corrected OCT angiographic images in real time, the averaging procedure used  $J = 3$  and  $K = 3$ ; the parameters for image registration were  $p = \pm 2$  and  $q = \pm 2$  in this work.

Figure 2 shows the flow chart for the GPU programming process. On the host PC, the captured spectral interference image ( $Nz = 1024$ : spectral size  $\times$   $Nx$ : lateral points, 16 bit) was transferred to the memory on the GPU. The data transfer rate between the host PC and the GPU device was increased using GPU paged memory. On the GPU, the data type of the spectral interference signal was first converted from a 16-bit integer to a 32-bit complex floating-point and then the spectrum was subtracted by the averaged spectrum. Next, zero-filling interpolation was performed with a forward Fourier transform, zero padded to increase the data-array length 2-fold ( $M = 2$ ).<sup>19</sup> The data were then inverse Fourier transformed back to the spectral domain and linearly interpolated into  $k$ -space. Here, only the constant values of linear interpolation were transferred to the GPU memory. The real and imaginary parts of the complex data were set to the processed data and zero, respectively. Next, the  $MNz$ -point FFT was executed for  $Nx$  lateral points. An amplitude image with  $Nz/2 \times Nx$  pixels was obtained. If this amplitude was larger than the threshold value that is 1 dB above the OCT intensity noise floor, then OCT angiography processing was performed using the previous amplitude of the OCT image. Because  $p = \pm 2$  and  $q = \pm 2$  were used for the BTM correction, a total of 25 OCT angiographic images were processed. The BTM-corrected OCT angiographic image had



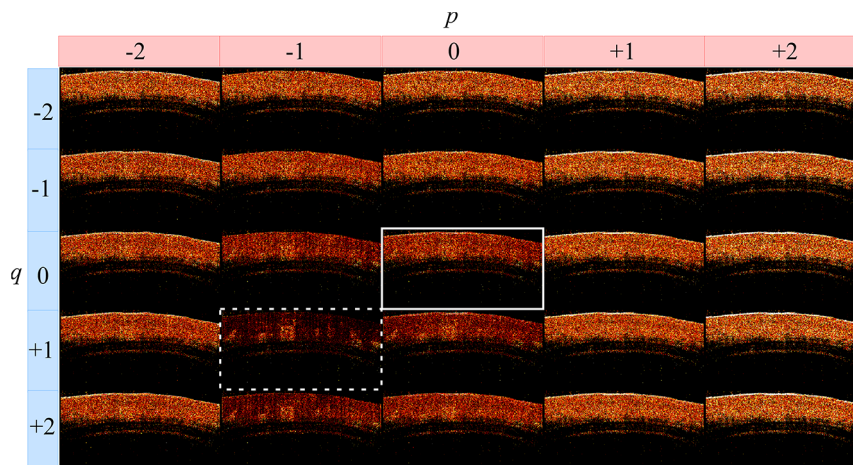


**Fig. 5** (a) OCT images of a human finger nail-fold region. The imaging range was  $4.8 \times 3.4 \text{ mm}^2$  ( $1024 \times 512$  pixels). (b), (d), and (f) OCT angiography using two OCT images without BTM correction (c), (e), and (g) IF-IBDV image. NR, nail root; BV, blood vessel.

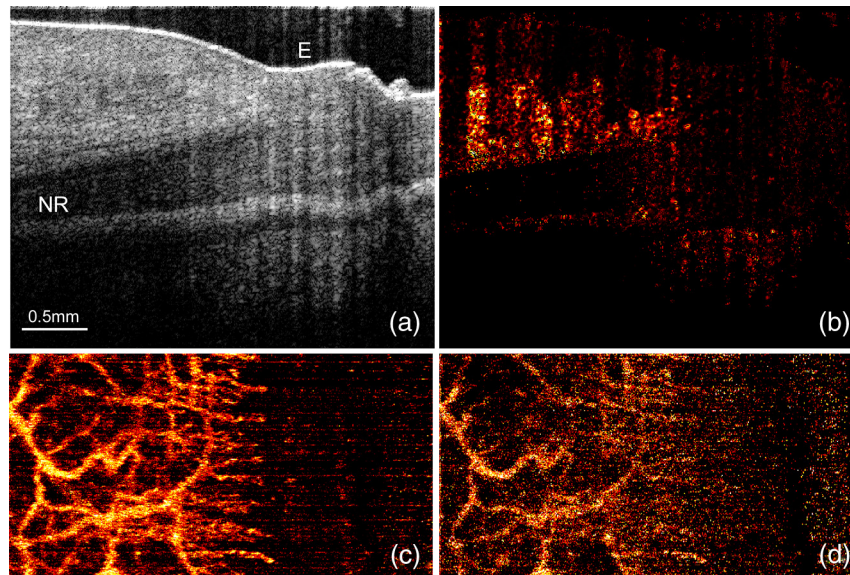
mode, only the image having the smallest total of pixel values is transferred to the host computer memory.

Finally, we estimated three-dimensional (3-D) OCT angiographic images using two frames and multiple frames. We measured the 3-D OCT data set of a human nail-fold region by adding slow scanning. This volume of data consists of 1000 frames with 512 A-lines/frame, and approximately 11 s was required to capture the entire 3D-OCT data volume. The

frame interval was  $1.6 \mu\text{m}$  and the corresponding sampling density level was 13.125. Figure 7(a) and 7(b) show the structural OCT image and OCT angiographic image, respectively. The image size was  $3.2 \times 2.5 \text{ mm}^2$  (lateral  $\times$  axial). Figure 7(c) and Video 2 show the maximum intensity projection (MIP) view and en face images of the 3D-OCT angiographic data set, respectively. The vasculature network can be clearly seen. Figure 7(d) shows the MIP image obtained from 3-D IF-IBDV images.<sup>16</sup>



**Fig. 6** Processed 25 OCT angiographic images for BTM correction. Solid square corresponds to the OCT angiogram in Fig. 5(d). Dash square indicates BTM-corrected OCT angiography. The video data, which consists of 50 images, was shown at the display rate of 44 fps (Video 1, QuickTime, 6.4 MB) [URL: <http://dx.doi.org/10.1117/1.JBO.19.2.021105.1>].



**Fig. 7** (a) OCT images of a human finger nail-fold region. The image size was  $3.2 \times 2.5 \text{ mm}^2$ . (b) OCT angiography, (c) MIP view and Video 2 en face images (QuickTime, 3.6 MB) [URL: <http://dx.doi.org/10.1117/1.JBO.19.2.021105.2>]. (d) MIP view from 3D IF-IBDV volume. NR, nail root; E, eponychium.

The small blood vessels could not be identified due to frame averaging. To perform OCT angiography using multiple frames, the 3-D data set must be obtained by driving the slow-axis scanner with a multiple-step function, which allows several OCT images to be averaged at the same position.<sup>17</sup> Moreover, all the frames required BTM correction on the order of a pixel. The speckle variance OCT angiography with a different BTM correction method using a different GPU has already been demonstrated.<sup>25</sup> In our next work, we are planning to compare various IB-OCT angiography algorithms and BTM correction methods on a GPU.

## 5 Conclusion

We demonstrated GPU-accelerated IB-OCT angiography by calculating the squared difference between two sequential frames with the simple BTM correction on the order of a pixel. Although the influence of a motion appeared in subsequent OCT angiographic images using multiple frames because of frame averaging, the two frames-based OCT angiography can reduce this influence. Our correction was performed by minimizing the sum of the pixel values using axial- and lateral-pixel-shifted structural OCT images. The BTM-corrected image was extracted from a total of 25 calculated OCT angiographic images. A GPU processing rate of more than 100 K lines/s was achieved, which exceeded the line rate of the camera (46.9 kHz). We demonstrated that our OCT system was capable of displaying structural OCT images and BTM-corrected OCT angiography in real time.

## Acknowledgments

This work was partially supported by JSPS KAKENHI Grant Number 25350519.

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